

WASTELESS PROCESSING OF RED MUD BY HYDROGARNET TECHNOLOGY

Rinat ABDULVALIYEV, Erbulat TASTANOV, Sergey GLADYSHEV, Kulzhaivk BEISEMBEKOVA, Nazym AKHMADIYEVA

Center of Earth Science, Metallurgy and Ore Beneficiation, Shevchenko St. 29/133, 050010, Almaty, Kazakhstan

rin-abd@mail.ru, nazym.akhmadiyeva@gmail.com

Abstract

The current alumina production of Kazakhstan by the consecutive Bayer-sintering process becomes less profitable and requires modernisation. We have developed technology, which allows wasteless recycling of red mud by a hydrochemical method with the possibility of obtaining gallium and vanadium and also non-alkali hydrogarnet mud, suitable for use in construction, and producing pig iron and titanium-containing slag. As raw material Kazakhstan's Koktalsk group gibbsite bauxite deposits with resources of 300 million tonnes was used. Red mud processing in an autoclave at 240 °C with liquor with high $\text{Na}_2\text{O}/\text{Al}_2\text{O}_3$ molar ratio in the presence of lime with obtaining of hydrogarnet mud, aluminium, sodium, vanadium and gallium concentrated in liquor. Removing aluminium was about 70 % and 95-98 % alkali. Liquor with medium $\text{Na}_2\text{O}/\text{Al}_2\text{O}_3$ molar ratio was conversed by adding $\text{Ca}(\text{OH})_2$ in liquor with high $\text{Na}_2\text{O}/\text{Al}_2\text{O}_3$ molar ratio by synthesis of tricalcium aluminate hydrate (TCAH), with subsequent decomposition in soda bicarbonate liquor. Decomposed liquor carbonised in two stages, it generates alumina-carbonate precipitate which proposed to extract gallium and vanadium. Hydrogarnet sludge almost doesn't contain alkali and consist less aluminium oxide and more calcium oxide than red mud. Direct reductive sintering of hydrogarnet mud mixed with charcoal without fluxing additive in a muffle furnace at 1600-1650 °C was studied. As a result of sintering was good separation products self arenaceous slag phase and iron. Extraction of iron in cast iron was 84.6 %.

Introduction

Kazakhstan has a large amount of research on the development hydroalkali method of processing red mud by hydrogarnet technology in recent years.¹

Treatment of red mud by autoclave leaching by the definite conditions using high modulus alkaline solution in the presence of lime and active multicomponent additive is synthesised of calcium compound - mostly ferruginous hydro-garnet

($3\text{CaO}\cdot\text{Fe}_2\text{O}_3\cdot 2\text{SiO}_2\cdot 2\text{H}_2\text{O}$), which doesn't contain aluminium and alkali. Its excludes formation of aluminium hydrogarnet ($3\text{CaO}\cdot\text{Al}_2\text{O}_3\cdot\text{SiO}_2\cdot 4\text{H}_2\text{O}$).^{2,3}

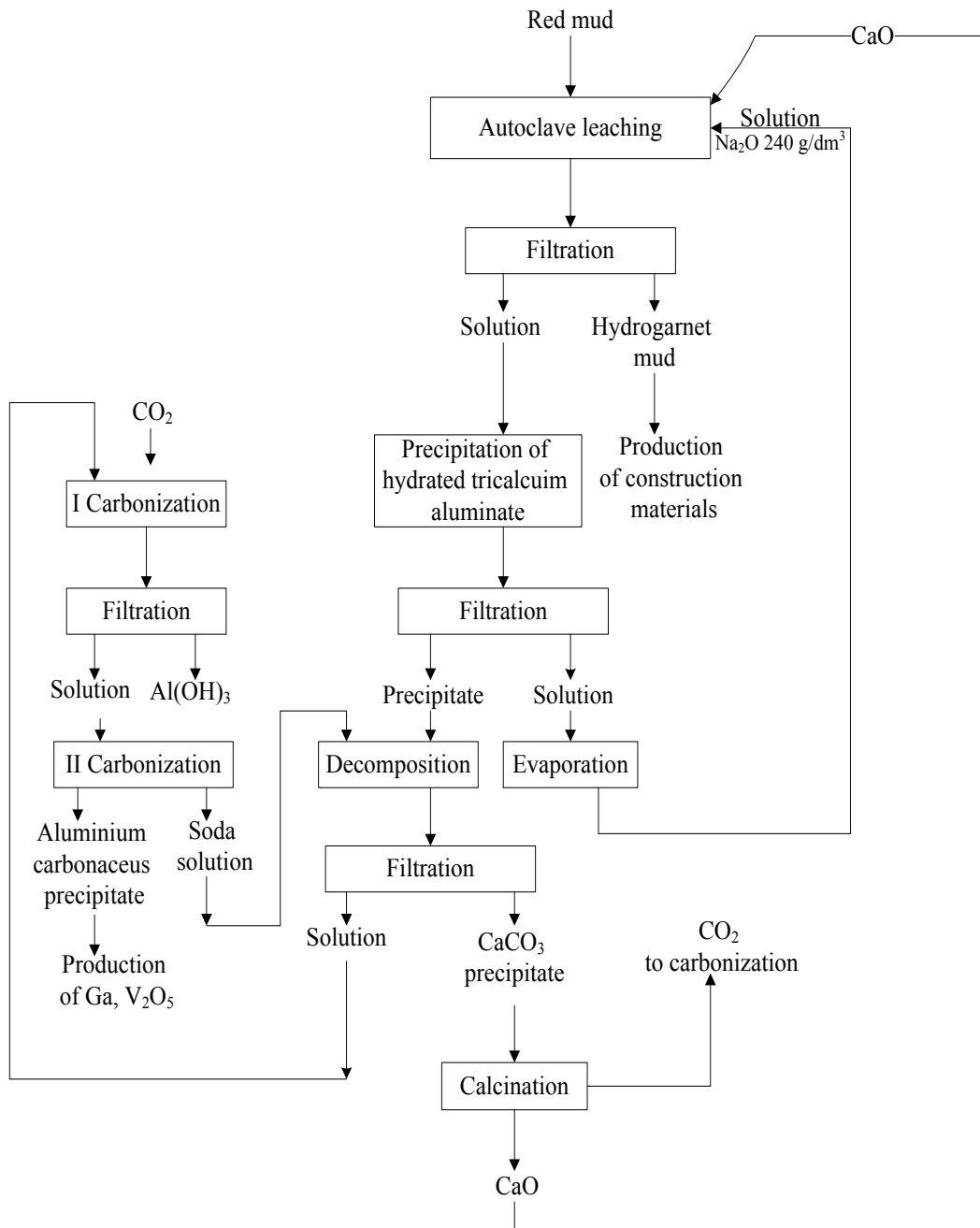


Figure 1: Technological scheme of hydro-garnet process for red mud

A red mud sample from Kocktalsk deposit (Republic of Kazakhstan) which was obtained by the Bayer process for high ferruginous bauxite was used in this study. Kocktalsk deposit bauxites rate as perspective raw material in alumina production.^{4,5}

The Kaktalsk deposit bauxites was determined to contain: 39.53 % Al₂O₃, 6.18 % SiO₂, 23.12 % Fe₂O₃, 4.37 % TiO₂ and 1.1 % CaO, $\mu=6.396$.

The red mud sample was determined to contain: 7.33 % NaO, 10.47 % Al₂O₃, 11.19 % SiO₂, 46.95 % Fe₂O₃, 7.9 % TiO₂, 6.33 % CaO.

A high-modulus solution (Na₂O 285.0, Na₂CO₃ 11.4, Al₂O₃ 14.65, SO₃ 4.23, SiO₂ 0.024, $\alpha_k = 32.0$) was used for autoclave leaching of red mud sample in the presence of lime-clinker suspension at a liquid-to-solids (L/S) ratio of 4.

As a result of autoclave leaching of red mud hydrogarnet sludge and middle modulus solution (165.35 g/dm³ Na₂O, 7.59 g/dm³ Na₂CO₃, 24.24 g/dm³ Al₂O₃, 3.52 g/dm³ SO₃, 0.05% SiO₂, $\alpha_k = 11.4$) was produced.

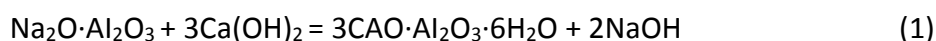
Table 1: XRD pattern of the hydrogarnet mud

Compound Name	Formula
Hematite	Fe ₂ O ₃
Andradite (hydrated)	Ca ₃ (Fe _{0.87} Al _{0.13}) ₂ (SiO ₄) _{1.65} (OH) _{5.4}
Katoite, syn	Ca ₃ Al ₂ (O ₄ H ₄) ₃
Magnetite, syn	Fe ₃ O ₄

As a result of autoclave leaching of red mud by hydrogranet technology 98 % Na₂O regenerated, 64.9 % of red mud was extracted to solution.

Extraction of hydrogarnet mud was 62.1 % of the initial bauxite.

Middle modulus solution converted by tricalcium hydroaluminat synthesis with Ca(OH)₂ according to the equation:



The effect of different temperatures from 40 to 100 °C was studied. The optimum conditions for synthesis of tricalcium hydroaluminat were found to be: 100 °C and 3-4 hours. Extraction of Al₂O₃ into tricalcium hydrogarnet was 64.2-64.6 %, α_k of the obtained solution was 30. Synthesised tricalcium hydroaluminat was analysed to contain 22.3 % Al₂O₃, 46.6 % CaO.

Tricalcium hydroaluminat decomposition carried out with 3 types of solution:

- alkali solution Na₂O 240 g/L
- sodium-alkali solution Na₂O 120 g/L and Na₂CO₃ 20 g/L
- soda solution Na₂CO₃ 60-160 g/L

Leaching carried out at 100 °C in temperature-controlled mixer for 180 minutes, and at 180 °C in autoclave for 90 minutes at L:S ratio of 4.

Leaching with sodium-alkali solution proceeds according to the equations:

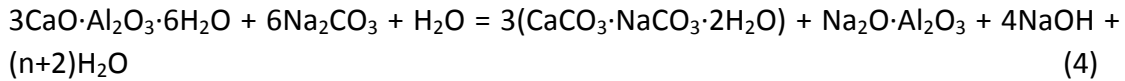
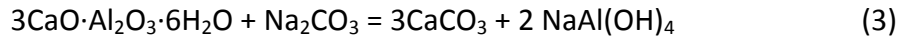
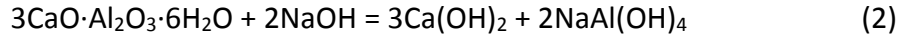


Table 2: Semi - quantitative analysis of tricalcium hydroaluminat leaching sediment at 180 °C

Compound Name	Formula
Calcite, syn	$\text{Ca}(\text{CO}_3)$
Unnamed_Hydrogarnet, syn	$(\text{CaO})_3(\text{Al}_2\text{O}_3)_{1.75}(\text{H}_2\text{O})_{3.75}$
Sodium Carbonate Oxide	Na_2CO_3

The optimum conditions for decomposition of tricalcium hydroaluminat were found to be: Na_2CO_3 concentration 140-160 g/dm³, 180 °C. Extraction of Al_2O_3 95-98.3 %. Direct smelting reduction of hydrogarnet mud mixed with charcoal without fluxing additive was studied to selective reduction of iron to obtain steel and slag. It was carried out at 1600-1650 °C at 1 hour.

Amount of charcoal was dosed to charge by on the basis of full reduction of iron oxides by the reactions:



There are studies on smelting reduction of Bayer red mud to separate iron in pig iron, and aluminium oxide, sodium, and titanium - in slag i.e. if content of iron oxides is 41.95 % in initial mud, for 100 g of mud 6.3 g of charcoal is necessary. Whereas, graphite crucible using, amount of charcoal was 75 % from calculated. 0.5 % of treacle as binding agent was added for dust-priming decreasing. It was briquetting at a pressure of 200 kg /cm², then dried in drying furnace at 350-400 °C for moisture

removal, which was added with treacle liquid. Obtained briquettes was strong enough.

Extraction ratio of pig iron was 35.0 % and slag was 37.5 %. Slag determined to contain 94.7 % Fe, 3.2 % Si, 1.8 % Ti, 0.52 % Al, 0.001 % P, 2.2 % C, 0.38 % Cr, 0.101 % Mn, 0.043 % Ni, 0.052 % Cu. Slag was divided into magnetic and nonmagnetic factions after magnetic separation. As a result 34.5 % magnetic and 66.0 % nonmagnetic factions separated.

Magnetic faction determined to contain 8.24 % Al_2O_3 , 14.57 % SiO_2 , 16.13 % CaO , 37.56 % Fe, 23.5 % TiO_2 . Nonmagnetic faction determined to contain 23.48 % Al_2O_3 , 20.3 % SiO_2 , 50.32 % CaO , 0.22 % Fe, 1.78 % TiO_2 .

Extraction of iron in pig iron was 88.0 %, in magnetic faction – 11.9 % and in nonmagnetic faction – 0.1 %.

Table 3: Magnetic faction of slag

Compound Name	Formula
Suessite	$(Fe_3Si)_{0.5}$
Wustite, syn	$Fe_{0.942}O$
Hongquiite, syn (NR)	$(TiO_{1.27})_{0.787}$
Iron	Fe
Aluminium Oxide	Al O
Quartz low, syn	SiO_2
Gehlenite, syn	$Ca_2Al_2SiO_7$
Andradite	$Ca_3Fe_{1.88}(SiO_4)_3$

Table 4: Nonmagnetic faction of slag

Compound Name	Formula
Calcio-olivine, syn	Ca_2SiO_4
Calcium Oxide	CaO
Gehlenite	$Ca_2Al_2SiO_7$
Aluminium Titanium	$AlTi_3$
Calcium Oxide	CaO_2

Table 5: The phase composition of pig iron

Compound Name	Formula
Iron	Fe
Iron Silicon	Fe _{0.9} Si _{0.1}
Moissanite-69R	SiC
Gupeiite, syn	Fe ₃ Si
Graphite	C

Conclusions

As a result of processing of red mud by hydrogarnet technology alkali regenerated into alkali-aluminate solution for 98.0 %, Al₂O₃ extraction ratio was 64.9 % and hydrogarnet mud –silicaferrous concentrate with high consumer properties.

The optimum conditions for synthesis of tricalcium hydroaluminate were found to be: 100 °C and 3-4 hours. Extraction of Al₂O₃ into tricalcium hydrogarnet was 64.2-64.6 %, α_k of the obtained solution was 30.

The optimum conditions for decomposition of tricalcium hydroaluminate were found to be: Na₂CO₃ concentration 140-160 g/l, 180 °C and 2 hours. Extraction rate of Al₂O₃ was 95-98.3 %.

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